

Analysis and Optimization of Coupled Windings in Magnetic Resonant Wireless Power Transfer Systems with Orthogonal Experiment Method

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Abstract—The coupled magnetic resonant unit (CMRU) has great effect on the transmitting power capability and efficiency of magnetic resonant wireless power transfer system. The key objective i.e. the efficiency coefficient k_Q is introduced in the design of CMRU or the coupled windings based on the mutual inductance model. Then the design method with orthogonal experiments and finite element method simulation is proposed to maximize the k_Q due to low precise analytical model of AC resistance and inductance for PCB windings at high-frequency. The method can reduce the design iterations and thereby can get more optimal design results. The experiments verified the design objective of k_Q as well as the design method effectively. In the optimal PCB windings prototype at operating frequency of 4 MHz, the k_Q and the maximum efficiency are increased by about 12 % and 4 % respectively.

Index Terms—Wireless power transfer; magnetic resonant; orthogonal experiments; magnetic coupling structure optimization.

I. INTRODUCTION

Medium-range efficient power transfer can be implemented through magnetic resonant wireless power transfer (MR-WPT), where the coupled windings resonate to exchange energy efficiently [1]–[5]. The coupled magnetic resonant unit (CMRU) consisting of coupled windings and compensation capacitances, as one of the key components in MR-WPT, has great effects on the system transmitting power capability, efficiency, distance, stability, etc. In the modelling (including the coupled mode theory and the circuit theory [6], [7]) and design of CMRU, the coupled winding parameters, such as AC resistance R_{ac} , inductance, or mutual inductance M should be required. Under high-frequency operation, the R_{ac} and M depends on the frequency greatly because of high-frequency eddy-current effect. There are some literatures [8]–[12] on the analytical modelling of the

transformer and inductor windings. In addition, they are available in the modelling and design of the coupled windings of CMRU [12]–[14]. But under higher operation frequency, such as several hundreds of kHz and MHz, the analytical modelling will have poor accuracy, especially for the coupled PCB windings characterized of much more fringing high-frequency magnetic field comparing with the magnetic-core transformer and inductor. In order to achieve an enough or higher accuracy, finite element method (FEM) simulation would be preferred. However, it will result in increasing simulation time greatly as for the optimal design of the coupled windings, especially with the method of the scanning parameters being available in FEM software. The method with single parameter analysis and FEM simulation [15], in which the influence of varying one parameter was studied while fixing all the other parameters, is utilized to simplify analysis and optimal design of the coupled windings. However, it will perhaps lose the best optimal design because there are interactions among the parameters. Therefore a method with orthogonal experiments and FEM simulation is proposed, and it is able to make trade-offs between design time and optimal solutions. The orthogonal experiment is one of optimal design methods, where only the representative experiments are selected [16].

The paper investigates the design objective based on the mutual inductance firstly, then analyses the interactions among the parameters and designs the orthogonal experiments, finally makes optimal design and verification.

II. MODEL OF CMRU AND THE DESIGN OBJECTIVE

The CMRU can be classified into two types: two winding structure and four winding structure [2]. The mutual inductance model for the four winding structure with series-connecting compensation capacitance is shown in Fig. 1. In the model, I_s and R_s is the high-frequency exciting source and its internal resistance; L_1 , L_2 , L_3 , and L_4 represent self-inductance of each winding respectively; C_1 , C_2 , C_3 , and C_4 represent series-connecting capacitance for each winding; R_1 , R_2 , R_3 , and R_4 represent the resistance of each winding

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under high-frequency current; M_{12} , M_{23} , and M_{34} represents mutual inductance between the two adjacent windings; R_L is the load resistance; $Z_i = R_i + jX_i$ represents the input impedance of the coupled magnetic unit; $Z'_i = R'_i + jX'_i$ represents impedance from the emitting winding port; $Z_o = R_o + jX_o$ represents equivalent load impedance from the load winding port. The efficiency of the MR-WPS with the four winding structure is divided into three parts η_{12} , η_{23} , and η_{34} as in Fig. 1. η_{12} , η_{23} , and η_{34} are the transmitting efficiency between the source and the emitting winding, the emitting winding and the receiving winding, the receiving winding and the load winding respectively.

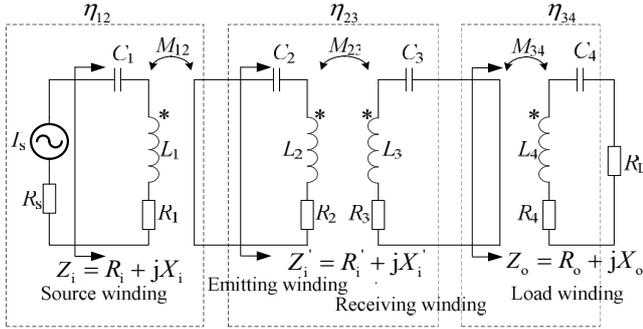


Fig. 1. Mutual inductance model of the four-winding structure.

In the design, both source compensation winding L_1 and load compensation winding L_4 are constructed with single turn to obtain small winding resistance R_1 and R_4 . Impedances Z_i , Z'_i and Z_o is purely resistive when each winding operates resonantly by design of source frequency and compensation capacitances, thus R_i , R'_i , and R_o can be written as follows:

$$\begin{cases} R_i = R_1 + \frac{(\omega_0 M_{12})^2}{R'_i} \approx \frac{(\omega_0 M_{12})^2}{R'_i}, \\ R'_i = R_2 + \frac{(\omega_0 M_{23})^2}{R_3 + R_o}, \\ R_o = \frac{(\omega_0 M_{34})^2}{R_4 + R_L} \approx \frac{(\omega_0 M_{34})^2}{R_L}, \end{cases} \quad (1)$$

ω_0 represents resonant frequency in the equation.

The total efficiency η of the CMRU can be expressed as a product of transmission efficiency between the two adjacent windings i.e. $\eta = \eta_{12}\eta_{23}\eta_{34}$, where $\eta_{12} \approx R_i / (R_s + R_i)$, $\eta_{34} \approx 1$ because of small winding resistance R_4

$$\eta_{23} = \frac{(\omega_0 M_{23})^2 R_o}{(R_3 + R_o)(R_2(R_3 + R_o) + (\omega_0 M_{23})^2)}. \quad (2)$$

When the equivalent load equal to optimal equivalent load resistance, $R_{o_opt} = \sqrt{R_3(\omega_0 M_{23})^2 / R_2 + R_3^2}$, η_{23} will be maximized as:

$$\eta_{23_max} = \frac{k_Q^2}{k_Q^2 + 2\sqrt{k_Q^2 + 1} + 2}, \quad (3)$$

$$k_Q = k_{23}\sqrt{Q_2 Q_3}, \quad (4)$$

where $k_{23} = M_{23} / \sqrt{L_2 L_3}$ represents the coupling coefficient between the emitting winding and the receiving winding; $Q_2 = \omega_0 L_2 / R_2$ and $Q_3 = \omega_0 L_3 / R_3$ represent the quality factor of the emitting and receiving windings respectively. It can be seen that, the maximum efficiency η_{23_max} only depends on k_Q determined by the intrinsic parameters k_{23} , Q_2 , and Q_3 of the windings.

The curve of Fig. 2 can be plotted from (3). It can be seen that, η_{23_max} will decrease with decreasing k_Q , and drops rapidly on the left side of the point a. Therefore, k_Q should be designed on the right side of point a if there are no limitations on selecting k_Q or the windings geometry. Moreover, if the k_Q has to be designed on the left side of point a due to some practical restrictions, it must be designed as large as possible for getting a high efficiency or high capability of power transmission. Here the k_Q is introduced to be as the design objective for the coupled windings.

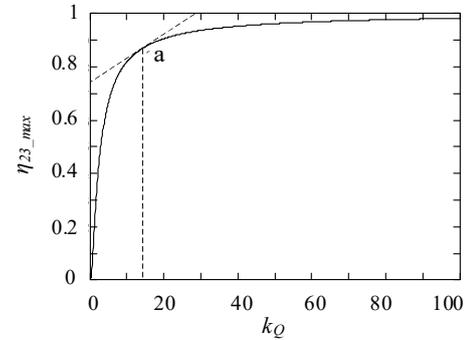


Fig. 2. Maximum efficiency η_{23_max} vs. k_Q .

Since η_{23} only denotes transmitting efficiency between the emitting winding and the receiving winding, the two-winding coupling structure, instead of the four-winding coupling structure, is adopted to verify the relationship between the maximum efficiency η_{23_max} and k_Q . As shown in Fig. 3, three pairs of coupling windings are constructed. In each pair of the coupling windings, the emitting winding and the receiving winding have the same diameter, which is 40 mm, 50 mm and 63 mm respectively; Both emitting winding and receiving winding are solenoid windings with number of turns of 10, solenoid length of 15 mm and wire diameter of 0.65 mm. The exciting current frequency is 3.9 MHz.

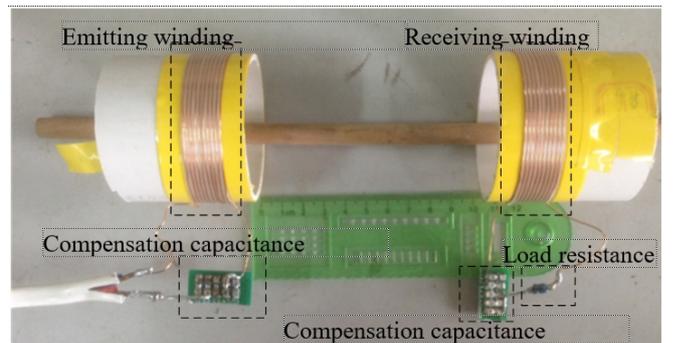


Fig. 3. Constructed windings for the model verification.

In order to compare the maximum efficiency of each pair under a same efficiency coefficient k_Q , corresponding

transmitting distance of the each pair for a same efficiency coefficient is calculated through (4) and the winding tested parameters listed in Table I (where L and R_{ac} represents self-inductance and equivalent AC resistance of the windings respectively, C represents compensation capacitance). Table II shows the calculating transmitting distance for the same efficiency coefficient.

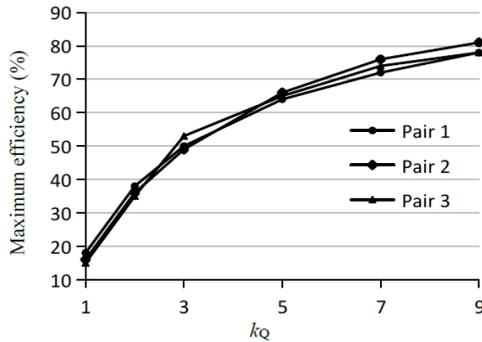
TABLE I. WINDING PARAMETERS OF EACH PAIR.

	Diameter (mm)	L (μH)	C (pF)	R_{ac} (Ω)
Pair 1	40	4.81	350	0.450
Pair 2	50	6.67	250	0.607
Pair 3	63	9.28	178	0.820

TABLE II. CORRESPONDING TRANSMITTING DISTANCE OF EACH PAIR FOR A SAME EFFICIENCY COEFFICIENT.

k_Q	9	5	3	2	1
Pair 1 (mm)	37	51	64	77	102
Pair 2 (mm)	47	64	81	96	127
Pair 3 (mm)	61	81	102	121	159

Changing transmitting distance of the each pair according to Table II and choosing the corresponding optimal equivalent load resistance R_{o_opt} to maximize the efficiency of each pair, then tested maximum efficiency of different pairs under different efficiency coefficient k_Q are shown in Fig. 4.

Fig. 4. Maximum efficiency of different pairs of windings vs. k_Q .

III. DESIGN WITH ORTHOGONAL EXPERIMENTS METHOD

A. Parameters Definition for Orthogonal Experiments

Using orthogonal experiment designing methods, the three

parameters named with index, factors, and levels should be defined [16]. In the optimal design of the PCB windings with the four-winding structure as shown in Fig. 5, the index is defined with k_Q .

It can be seen that the maximum efficiency of the different pairs will keep the same as long as their efficiency coefficient is the same, i.e. the maximum efficiency only depends on k_Q . Moreover, the maximum efficiency increases with k_Q . It should be noted that small difference (maximum difference is about 5 %) of the tested maximum efficiencies for a same k_Q is caused by testing error and parasitic parameters, such as self-capacitance of the windings etc.

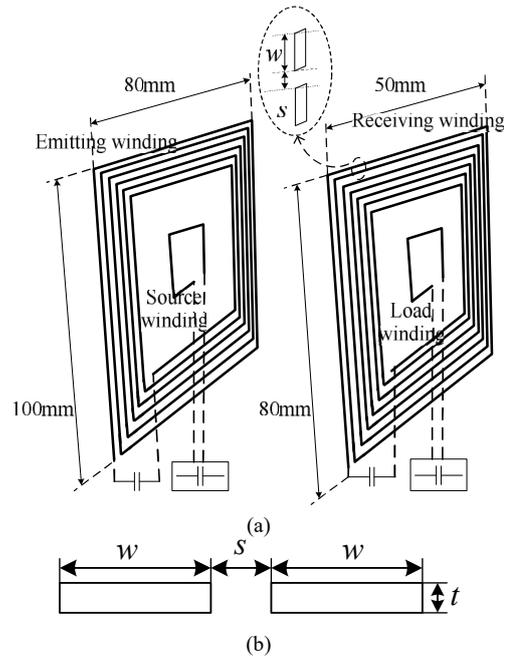
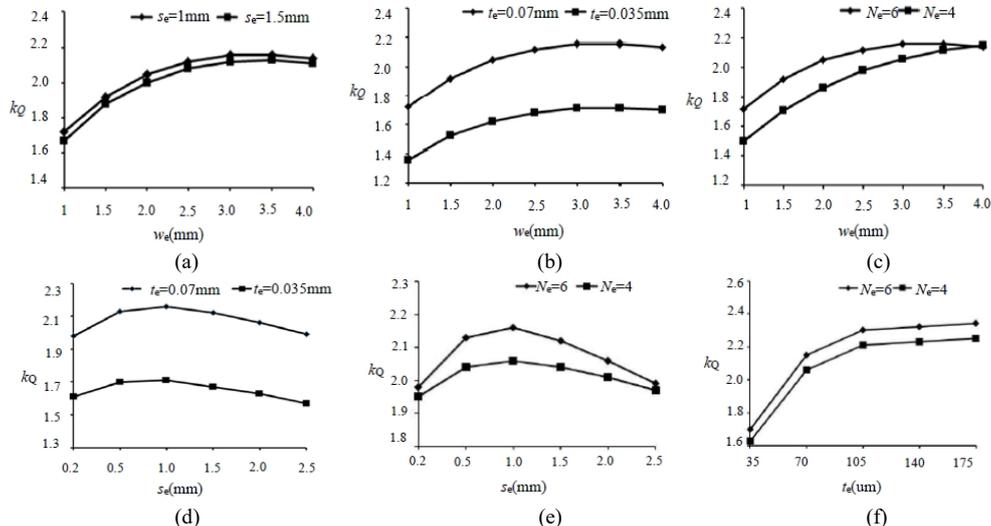


Fig. 5. Winding structure: a) Four-winding structure with PCB winding; b) PCB trace.

The factors are defined with geometrical parameters of the windings, including winding's number of turns N , the trace width w , the distance between adjacent traces s , and the trace thickness t . The levels are defined with the value of the factors or the geometrical parameters such as the s can be given three different values with 0.5 mm, 1 mm and 1.5 mm, respectively.

Fig. 6. Interactions analysis among the parameters or factors N_e , w_e , s_e , and t_e : a) k_Q vs. w_e and s_e ; b) k_Q vs. w_e and t_e ; c) k_Q vs. w_e and N_e ; d) k_Q vs. s_e and t_e ; e) k_Q vs. s_e and N_e ; f) k_Q vs. t_e and N_e .

In the optimal design of the PCB windings, the constraints are maximum size of the emitting winding with width 80 mm and length 100 mm and the receiving winding with width 50 mm and length 80 mm. And the transmitting distance is fixed to 130 mm; source frequency is 4 MHz.

B. Interaction Analysis of the Factors

The factors include the winding geometrical parameters of N_e , w_e , s_e , and t_e for the emitting winding. Here the subscript represents the parameters for the emitting winding. In order to get the orthogonal chart for orthogonal experiments, the interactions among the parameters is analysed. Using the eddy current field simulator from the FEM software Ansoft, the factor interactions of the emitting winding can be obtained as plotted in Fig. 6. In accordance with the judgment of orthogonal experiments and Fig. 6, it can be found that there are no or weak interactions between w_e and s_e , w_e and t_e , s_e and t_e , s_e and N_e , t_e and N_e , but there exists strong interactions between N_e and w_e . The same analysis and conclusions can be made to the receiving winding.

C. Orthogonal Experiment Design

In initial designs, given that t_e has three levels with 1 oz (1 oz = 35 μ m), 2 oz, and 3 oz, Fig. 6 shows that t_e has no interaction with the other factors N_e , w_e and s_e , and Fig. 6(f) also shows that k_Q increases slightly with increasing of t_e at above 2 oz, while expense will increase greatly. Then t_e is

fixed as 2 oz in the whole design, i.e t_e has only one level. So t_e can be excluded from the factors in the design of orthogonal chart, resulting in reducing numbers of experiments. There are 6 factors (including N_e , w_e , s_e for the emitting winding and N_r , w_r , s_r for the receiving winding) and the each factor has 3 levels as given in Table III.

Considering the interaction factors (N_e with w_e , and N_r with w_r), the orthogonal chart $L_{27} (3^{13})$ is designed as Table IV. Table IV shows that there are 27 representative experiments totally; Except for the experiment number n , the “1”, “2” and “3” represent ‘level 1’, ‘level 2’ and ‘level 3’ of each factor as listed in Table III; The order of factors is determined by referring to [16] (“ \times ” is the notation of interaction). The index of the calculated “ k_Q ” is listed in the Table IV for each representative experiment by substituting AC resistance and mutual inductance of the windings obtained by FEM simulations into (4).

TABLE III. LEVELS CHART OF FACTORS.

	level 1	level 2	level 3
N_e (turns)	6	7	5
N_r (turns)	6	4	5
w_e (mm)	3.5	2.5	3
w_r (mm)	3	2	2.5
s_e (mm)	1.5	0.5	1
s_r (mm)	0.2	0.5	1

TABLE IV. $L_{27} (3^{13})$ ORTHOGONAL CHART.

Level	Factors														k_Q
	N_e	N_r	s_e	s_r	w_e	$N \times w$	$N_e \times w_e$	null	w_r	null	null	$N_r \times w_r$	null		
n	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1.86
	2	1	1	1	1	2	2	2	2	2	2	2	2	2	1.99
	3	1	1	1	1	3	3	3	3	3	3	3	3	3	1.97
	4	1	2	2	2	1	1	1	2	2	2	3	3	3	2.06
	5	1	2	2	2	2	2	2	3	3	3	1	1	1	2.11
	6	1	2	2	2	3	3	3	1	1	1	2	2	2	2.16
	7	1	3	3	3	1	1	1	3	3	3	2	2	2	2.15
	8	1	3	3	3	2	2	2	1	1	1	3	3	3	2.08
	9	1	3	3	3	3	3	3	2	2	2	1	1	1	2.12
	10	2	1	2	3	1	2	3	1	2	3	1	2	3	2.04
	11	2	1	2	3	2	3	1	2	3	1	2	3	1	2.05
	12	2	1	2	3	3	1	2	3	1	2	3	1	2	1.91
	13	2	2	3	1	1	2	3	2	3	1	3	1	2	2.05
	14	2	2	3	1	2	3	1	3	1	2	1	2	3	2.09
	15	2	2	3	1	3	1	2	1	2	3	2	3	1	2.03
	16	2	3	1	2	1	2	3	3	1	2	2	3	1	1.95
	17	2	3	1	2	2	3	1	1	2	3	3	1	2	2.08
	18	2	3	1	2	3	1	2	2	3	1	1	2	3	2.11
	19	3	1	3	2	1	3	2	1	3	2	1	3	2	2.13
	20	3	1	3	2	2	1	3	2	1	3	2	1	3	1.90
	21	3	1	3	2	3	2	1	3	2	1	3	2	1	2.15
	22	3	2	1	3	1	3	2	2	1	3	3	2	1	2.16
	23	3	2	1	3	2	1	3	3	2	1	1	3	2	1.97
	24	3	2	1	3	3	2	1	1	3	2	2	1	3	2.09
	25	3	3	2	1	1	3	2	3	2	1	2	1	3	2.05
	26	3	3	2	1	2	1	3	1	3	2	3	2	1	1.97
	27	3	3	2	1	3	2	1	2	1	3	1	3	2	1.98
K_1	18.49	18.00	18.18	18.00	18.45	17.95	18.51	18.44	18.08	18.46	18.40	18.17	18.39		
K_2	18.30	18.71	18.32	18.64	18.23	18.45	18.55	18.41	18.48	18.32	18.36	18.81	18.41		
K_3	18.39	18.49	18.69	18.55	18.51	18.80	18.13	18.34	18.63	18.41	18.44	18.22	18.39		
R	0.19	0.71	0.51	0.64	0.28	0.85	0.42	0.09	0.55	0.14	0.08	0.64	0.03		

Notes: n means the number of experiments. K_i is relative index, and R is the range of the factor in the same column.

According to the design of orthogonal experiments with analysis of K_1, K_2, K_3 , and R (K_1, K_2, K_3 are relative index, and R is the range of the factor in the same column), the optimal PCB windings can be got as follows, $N_e = 5, N_r = 4, s_e = 1 \text{ mm}, s_r = 0.5 \text{ mm}, w_e = 3.5 \text{ mm}, w_r = 3 \text{ mm}, t_e = t_r = 0.07 \text{ mm}$. While the optimal design with the control variables of [15] is $N_e = 6, N_r = 5, s_e = 1 \text{ mm}, s_r = 0.5 \text{ mm}, w_e = 3 \text{ mm}, w_r = 2 \text{ mm}, t_e = t_r = 0.07 \text{ mm}$.

IV. EXPERIMENTAL TEST

In order to verify the theoretical analysis above, the PCB windings prototypes based on the method in [15] and the proposed orthogonal experiment designing method are constructed and thereby illustrated in Fig. 7(a) and Fig. 7(b), respectively.

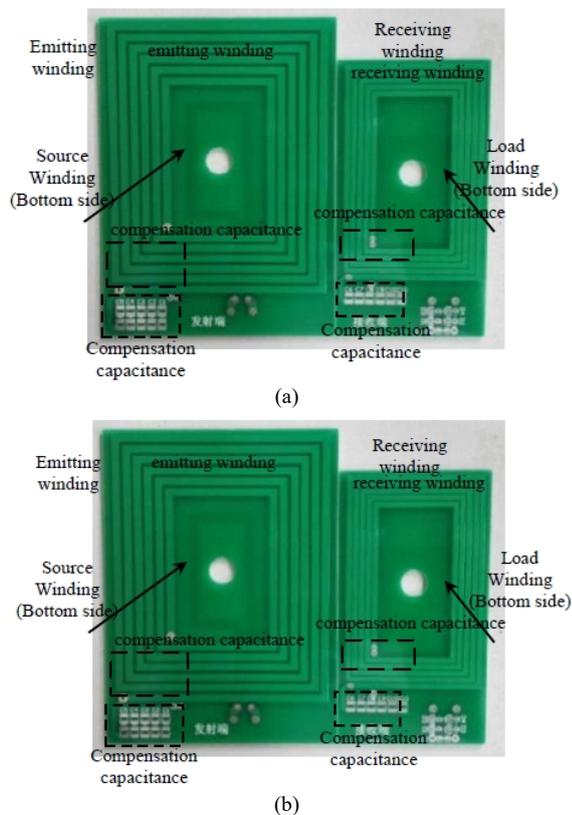


Fig. 7. Constructed windings prototypes: a) Windings optimized by method in [15]; b) Windings optimized by the orthogonal experiments.

The winding parameters AC resistance R_{ac} and mutual inductance M measured by Impedance Analyzer WK-6500B at 4 MHz frequency are given in Table V and Table VI.

TABLE V. PARAMETERS OF WINDINGS OPTIMIZED BY METHOD IN [15].

Frequency at 4 MHz	R_{ac}	M	k_Q
Emitting winding	361 m Ω	30.7 nH	2.19
Receiving winding	343 m Ω		

TABLE VI. PARAMETERS OF WINDINGS OPTIMIZED BY ORTHOGONAL EXPERIMENTS.

Frequency at 4 MHz	R_{ac}	M	k_Q
Emitting winding	255 m Ω	21.0 nH	2.46
Receiving winding	181 m Ω		

It shows that k_Q from (4) with the test winding parameter is increased by about 12 %. Then, the maximum efficiency from (3) is 41.3 % and 45.2 % respectively, and the efficiency increases by about 4 %.

V. CONCLUSIONS

The CMRU is a key component of the MR-WPT, and its maximum transmitting efficiency only depends on the k_Q determined by the intrinsic parameters, i.e. the windings coupled coefficient and its quality factor. The efficiency will decrease with decreasing k_Q , and drops rapidly before the key k_Q . The introducing of k_Q as design objective of the CMRU aims to the maximum efficiency. And in order to improve the efficiency, the k_Q must be optimized as large as possible by the windings geometry.

The proposed design method with orthogonal experiment and FEM simulation is for optimizing the coupled windings, especially the air-core PCB winding characterized of much more fringing magnetic field, excited by high-frequency source which is up to several hundreds of kHz. In the method, the k_Q is defined to be as the index for optimizing objective, and the factors includes the winding turn numbers, the PCB trace width, and the distance between adjacent traces. But there only exists interaction between the winding turn numbers and the trace width, resulting in the small numbers of experiments.

The proposed design method not only optimizes the PCB windings to get high k_Q effectively, but also reduces the numbers of experiments greatly. The PCB winding design example shows that the k_Q was optimized to be increased by about 12 %, resulting in improving the maximum efficiency by about 4 %. The experiments and FEM simulation verified the analysis and the design method.

REFERENCES

- [1] A. Kurs, *et al*, "Wireless energy transfer via strongly coupled magnetic resonances", *Science*, vol. 317, pp. 83–85, 2007. [Online]. Available: <http://dx.doi.org/10.1126/science.1143254>
- [2] Zhao Zhengming, Zhang Yiming, Chen Kainan, "New progress of magnetically-coupled resonant wireless power transfer technology", in *Proc. CSEE.*, 2013, pp. 1–13. [Online]. Available: <http://dx.doi.org/10.13334/j.0258-8013.pcsee.2013.03.003>
- [3] S. Hui, W. Zhong, C. Lee, "A critical review of recent progress in mid-range wireless power transfer", *IEEE Trans. on Power Electronics*, vol. PP, pp. 1–1, 2013. [Online]. Available: <http://dx.doi.org/10.1109/TPEL.2013.2249670>
- [4] U. K. Madawala, M. Neath, D. J. Thrimawithana, "A power-frequency controller for bidirectional inductive power transfer systems", *IEEE Trans. Industrial Electronics*, vol. 60, pp. 310–317, 2013. [Online]. Available: <http://dx.doi.org/10.1109/TIE.2011.2174537>
- [5] Dac-Binh Ha, Duc-Dung Tran, Vu Tran-Ha, Een-Kee Hong, "Performance of amplify-and-forward relaying with wireless power transfer over dissimilar channels", *Elektronika ir Elektrotechnika*, vol. 21, no. 5, pp. 91–95, 2015. [Online]. Available: <http://dx.doi.org/10.1109/63.750181>
- [6] S. Cheon, Y. H. Kim, S. Y. Kang, *et al*, "Circuit-model-based analysis of a wireless energy-transfer system via coupled magnetic resonances", *IEEE Trans I.E.*, vol. 58, no. 7, pp. 2906–2914, 2011. [Online]. Available: <http://dx.doi.org/10.1109/TIE.2010.2072893>
- [7] Hongchang Li, Kangping Wang, Lang Huang, *et al* "Dynamic modeling based on coupled modes for wireless power transfer systems", *IEEE Trans on P.E.*, vol. 30, no. 11, pp. 6245–6253, 2015. [Online]. Available: <http://dx.doi.org/10.1109/TPEL.2014.2376474>
- [8] J. A. Ferreira, "Improved analytical modeling of conductive losses in magnetic components", *IEEE Trans. P. E.*, vol. 9, no. 1, pp. 127–131,

1994. [Online]. Available: <http://dx.doi.org/10.1109/63.285503>
- [9] R. Sullivan Charles, "Optimal choice for number of strands in a litz-wire transformer winding", *IEEE Trans. P. E.*, vol. 14, no. 2, pp. 283-291, 1999. [Online]. Available: <http://dx.doi.org/10.1109/63.750181>
- [10] R. P. Wojda, M. K. Kazimierczuk, "Analytical optimization of solid-round-wire windings", *IEEE Trans. on IE*, vol. 60, no. 3, pp. 1033-1041, 2013. [Online]. Available: <http://dx.doi.org/10.1109/TIE.2012.2189543>
- [11] I. Lope, C. Carretero, J. Acero, *et al.*, "AC power losses model for planar windings with rectangular cross-sectional conductors", *IEEE Trans. P.E.*, vol. 29, no. 1, pp. 23-28, 2014. [Online]. Available: <http://dx.doi.org/10.1109/TPEL.2013.2256928>
- [12] Z. Pantic, S. Lukic, "Computationally-efficient, generalized expressions for the proximity-effect in multi-layer, multi-turn tubular coils for wireless power transfer systems", *IEEE Trans. Magnetics*, vol. 49, no. 11, pp. 5404-5416, 2013. [Online]. Available: <http://dx.doi.org/10.1109/TMAG.2013.2264486>
- [13] Z. Wang, X. Z. Wei, H. F. Dai, "Nested three-layer optimization method for magnetic coils used in 3kW vehicle-mounted wireless power transfer system", *IET Power Electronics*, vol. 9, no. 13, pp. 2562-2570, 2016. [Online]. Available: <http://dx.doi.org/10.1049/iet-pel.2015.0840>
- [14] S. R. Cove, M. Ordonez, "Wireless-power-transfer planar spiral winding design applying track width ratio", *IEEE Trans. I. A.*, vol. 51, no. 3, pp. 2423-2433, 2015. [Online]. Available: <http://dx.doi.org/10.1109/TIA.2014.2372092>
- [15] H. Jiang, S. X. Liang, J. M. Zhang, *et al.*, "Design and optimization of printed spiral coils in wireless power transfer for biomedical implants", *4th Int. Conf. Biomedical Engineering and Informatics*, 2011, pp. 1064-1067. [Online]. Available: <http://dx.doi.org/10.1109/BMEI.2011.6098398>
- [16] L. Feibao, L. Shulong, X. Meiyu, L. Wenli, *Methods of applied statistics*. Beijing: Peking University Press, 2010, pp. 164-187.